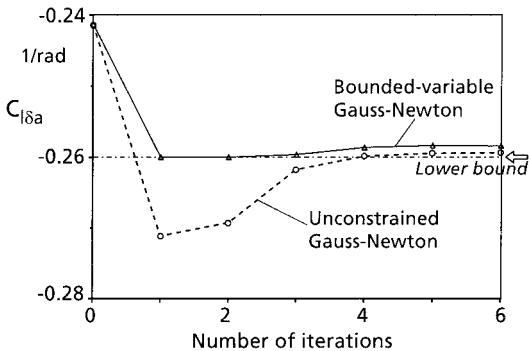
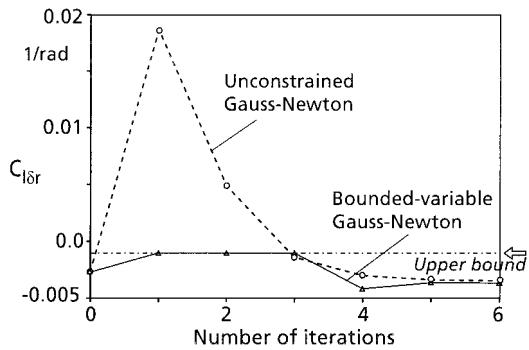


a) Dihedral effect



b) Aileron effectiveness



c) Rolling moment caused by rudder deflection

Fig. 1 Iterative estimates of typical rolling moment derivatives.

immediately by indications to leave the active set, can result, particularly as the minimum of the cost function is approached. The reason for this is twofold: 1) the roundoff errors becoming dominant, and the gradients computed using the numerical approximations are inaccurate; and 2) some variables are approximately linearly dependent. This phenomenon was, however, not encountered in several examples of estimating nonlinear aerodynamic parameters with various degrees of complexity.

Conclusion

The widely used Gauss-Newton method for aircraft parameter estimation in the time domain has been successfully extended to account for simple bounds on the variables. From an engineer's point of view and for implementation purposes, the active set strategy appears to be a simple, direct, and efficient approach. Additionally, the approach retains all of the advantages of the classical unconstrained Gauss-Newton at marginally larger computational overhead. The method extends, in general, the scope of aircraft parameter estimation by permitting the limitation of the variables to be estimated within a specified range. The performance of the bounded-variable Gauss-Newton method presented in this Note was demonstrated on a typical example of estimating the stability and control derivatives pertaining to the lateral-directional motion of an aircraft from flight data.

References

- ¹Hamel, P. G., and Jategaonkar, R. V., "Evolution of Flight Vehicle System Identification," *Journal of Aircraft*, Vol. 33, No. 1, 1996, pp. 9-28.
- ²Klein, V., "Estimation of Aircraft Aerodynamic Parameters from Flight Data," *Progress in Aerospace Sciences*, Vol. 26, Pergamon, Oxford, England, U.K., 1989, pp. 1-77.
- ³Maine, R. E., and Iliff, K. W., "Identification of Dynamic Systems—Applications to Aircraft. Part 1: The Output Error Approach," AGARD, AG-300, Vol. 3, Pt. 1, Neuilly-sur-Seine, France, Dec. 1986.
- ⁴Oswald, W. B., "General Formulas and Charts for the Calculation of Airplane Performance," NACA Rept. 408, Jan. 1932.
- ⁵Weiss, S., Gockel, W., Mönnich, W., and Rohlf, D., "Identification of Dornier-328 Reversible Flight Control Systems," AIAA Paper 98-4163, Aug. 1998.
- ⁶Jategaonkar, R. V., and Plaetschke, E., "Algorithms for Aircraft Parameter Estimation Accounting for Process and Measurement Noise," *Journal of Aircraft*, Vol. 26, No. 4, 1989, pp. 360-372.
- ⁷Rao, S. S., *Engineering Optimization: Theory and Practice*, Wiley, New York, 1996, pp. 333-351.
- ⁸Jacob, H. G., "An Engineering Optimization Method with Application to STOL-Aircraft Approach and Landing Trajectories," NASA TN D-6978, Sept. 1972.
- ⁹Jategaonkar, R. V., and Plaetschke, E., "Non-Linear Parameter Estimation from Flight Data Using Minimum Search Methods," DFVLR-FB 83-15, Braunschweig, Germany, March 1983.
- ¹⁰Murphy, P. C., "A Methodology for Airplane Parameter Estimation and Confidence Interval Determination of Nonlinear Estimation Problems," NASA RP 1153, April 1986.
- ¹¹Byrd, R. H., Lu, P., Nocedal, J., and Zhu, C., "A Limited Memory Algorithm for Bound Constrained Optimization," *SIAM Journal of Scientific Computing*, Vol. 16, No. 5, 1995, pp. 1190-1208.
- ¹²Gill, P. E., and Murray, W., "Minimization Subject to Bounds on the Variables," National Physical Lab. Rept. NAC 72, Middlesex, England, Dec. 1976.
- ¹³Stark, P. B., and Parker, R. L., "Bounded Variable Least Squares: An Algorithm and Applications," *Journal of Computational Statistics*, Vol. 10, No. 2, 1995, pp. 129-141.
- ¹⁴Jategaonkar, R. V., Mönnich, W., Fischenberg, D., and Krag, B., "Identification of C-160 Simulator Data Base from Flight Data," *Proceedings of the 10th IFAC Symposium on System Identification*, Elsevier, IFAC Publ., Oxford, England, UK, 1994, pp. 1031-1038.

Errata

Implications of the Insensitivity of Vortex Lift to Sweep

Lance W. Traub
Texas A&M University, College Station, Texas 77843-3141

[J. Aircraft 37 (3), pp. 531-532 (2000)]

Equation (6) should be:

$$C_{Pv}(x, y) = 1 - \left(4.63 \tan^{1.2} \alpha \cos \alpha \left(\frac{2s}{b} \right) \right. \\ \left. \times \cos^2 \left\{ \tan^{-1} \left(\frac{1}{z_v} \left(\frac{y}{s} - y_v \right) \right) \right\} \right) \left/ 2\pi z_v \tan^{0.2} \epsilon \right.^2$$

On page 532, the second sentence of the last paragraph should read: "This may be considered an upper (or rearward) bound as the wing sweep tends to 90 deg and the wing's trailing-edge extent tends to 0."